Bar US Corporation ISO 15835 TESTS ON BAR-US SIMGRIP LT REINFORCING BAR MECHANICAL SPLICES ASSEMBLED WITH BS4449 GRADE 460B REINFORCING BAR

Miami, Florida





Final Report January 5, 2010 WJE No. 2009.5202.B

Prepared for: Bar-US Corporation

Prepared by:

Wiss, Janney, Elstner Associates, Inc. IAS Accredited Laboratory



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Miami, Florida

Scott K. Graham Project Manager

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Final Report

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Mıami, Florida

INTRODUCTION

Wiss, Janney, Elstner Associates, Inc. (WJE) has conducted a series of tensile tests and reversed-loading low cycle tests on a reinforcing bar mechanical splice system for Bar-US Corporation (Bar-US). The tests were conducted on the Simgrip LT mechanical splices in metric bar size Nos. 20, 32 and 40 assembled using BS4449:1997 Grade 460B reinforcing bar. The tests were conducted in general accordance with ISO 15835-1 "Steels for the Reinforcement of Concrete - Reinforcement Couplers for Mechanical Splices of Bars - Part 1: Requirements" (2009) and ISO 15835-2 "Steels for the Reinforcement of Concrete - Reinforcement Couplers for Mechanical Splices of Bars - Part 2: Test Methods" (2009). The intent of the testing is to provide test data on splices assembled using BS4449 Grade 460 reinforcement, to be submitted to various authorities who are reviewing the splice system as part of these authorities' product review and acceptance process.

Unspliced control bar specimens were also tested. For each bar size, the control bars came from the same lots of bar that were used to make the splice specimens, which were assembled using Grade 460B reinforcing bar manufactured according to the requirements of "Specification for carbon steel bars for the reinforcement of concrete, BS4449:1997. The control bar tests were performed to determine the yield strength, yield strain, tensile strength, and final elongation of the unspliced reinforcing bar. The results of the control bar tests were compared to the tensile requirements of BS4449:1997.

DESCRIPTION OF THE SPLICE SYSTEM

Bar-US Simgrip LT Splice System

The Simgrip LT splice system consists of various components that are assembled together to form a splice. The standard splice consists of three components: two pieces of reinforcing bar and one threaded steel coupling devices. One end of each piece of reinforcing bar is cut square and placed into a machine that upsets or enlarges the end of the bar. Threads are then formed onto the upset ends of the reinforcing bars. One bar has threads cut over a longer length to allow for position splicing. Final assembly of the

splice takes place in the field or in the shop by engaging the upset and threaded ends of the reinforcing bars into the threaded Simgrip LT coupling sleeve. An illustration of a splice assembly is shown in Figure 1.



Figure 1. Schematic illustration of the Simgrip LT splice system. Note: product as tested did not include the locknut.



TEST PLAN, SPECIMEN ASSEMBLY AND TEST PROCEDURES

Test Plan

The test plan was made in general accordance with the testing requirements of ISO 15835-1. Table A.1 in ISO 15835-1 specifies that qualification testing of a mechanical splice system consist of tests performed

on three samples of the largest size, three samples of a medium size and three samples of the smallest size. At the request of Bar-US, tests were planned for Simgrip LT splices assembled with reinforcing bar size Nos. 20, 32 and 40 and companion unspliced control bars in the same bar sizes. A summary of the test plan matrix is shown in Table 1.

Table 1- Test Plan Matrix Bar ISO 15835 Specimens **Control** Size **Specimens** No. **Unspliced BS4449** Category B Category S2 **Tensile** Low Cycle Grade 460B Test Test **Reinforcing Bar** 20 3 3 32 3 3 1 40 3 3 1

Control Bar Specimens and Reinforcing Bar Sources

Bar-US provided WJE with the unspliced control bar specimens. Bar-US indicated to WJE that all of the pieces of reinforcing bar in a given size came from the same lot of reinforcing steel. Bar-US also indicated that the reinforcing bars provided were procured as conforming to BS4449:1997 Grade 460B. Reinforcing bar mill certificates are provided in Appendix A.

Procedures for Control Bar Tensile Tests

Unspliced control bar specimens were tested monotonically in axial tension in accordance with "Steel for reinforcement and prestressing of concrete - Test methods Part 1: Reinforcing bars, wire rod and wire," ISO 15630-01:2002. A clip-on strain extensometer measured the elongation of each unspliced control bar test specimen. The electrical signal output from the clip-on strain extensometer and an electrical signal indication of the test machine load were recorded digitally using a computer. Force-elongation plots for all control bar specimens were produced by plotting the digital record. For the unspliced bar specimens, the gage length of the clip-on strain gage was 100 mm.

Percent total elongation at maximum force (A_{gt}) was measured on each bar after fracture as prescribed in ISO 15630-01 Section 5.3. A_{gt} was determined by first scribing a series of gage marks onto the central length of the untested specimen at 20 mm intervals over a total length of at least 100 mm. After the test, a measurement was made of the distance between two scribe points, at least 50 mm or two times the bar diameter (whichever is greater) from the fracture and having an original gage length of 100 mm. As specified by ISO 15630-01, A_{gt} was calculated as the percentage increase in length of the gage length plus the percent elastic elongation represented by the tensile strength R_m divided by Young's modulus. A similar measurement was made to obtain A_5 by measuring the distance between two scribe points having an original gage length of five times the diameter of the bar and centered across the fracture.

Procedures for Category B Tensile Tests

A monotonically increasing tensile load was applied until failure in accordance with Section 5.3 of ISO 15835-2. The test machine was operated under displacement control. The elongation (slip) across the splice was recorded until approximately 120 percent of actual bar yield was reached. The LVDT frame was subsequently removed from the specimen so that the instrument would not be damaged when the specimen fractured. For safety purposes, the test machine was temporarily paused with displacement held



constant when an instrument was removed from the test specimen. After removal of the instrumentation, displacement was increased until the specimen fractured. The peak load indicated by the test machine and the observed type of fracture were recorded for each specimen. Corresponding stresses were determined using the nominal bar area. Measurements of total elongation at maximum force (A_{gt}) were made on the bars after fracture using the methods specified in ISO 15630-01 Section 5.3.

Procedures for Category S2 Low Cycle Tests

Category S2 reversed-load cyclic tests utilized the loading protocol shown in Table 2, as established by ISO 15835-2 Section 5.6.2. In the table, $R_{eH, spec}$ is the specified minimum yield strength of the reinforcing bar, and ε_y is the strain of the reinforcing bar at the specified yield stress calculated using a Young's Modulus of 2 x 10^5 MPa.

Table 2 - ISO 15835 Cate	egory S2 testing protocol
---------------------------------	---------------------------

Load Stage	Tension Elongation	Compression Force	No. of Cycles
1	$2 \epsilon_{ m y} L_{ m g}$	0.5 R _{eH, spec}	4
2	$5 \epsilon_{ m y} L_{ m g}$	0.5 R _{eH, spec}	4
3	Load in	monotonic tension to	failure

Elongation (slip) across the splice was monitored during Stages 1, 2, and 3 by a pair of LVDTs installed in a frame having a fixed gage length of 200, 400 or 500 mm depending on the reinforcing bar size. Strain in the reinforcing bar was monitored for reference purposes during Stages 1, 2, and 3 at a point away from the splice affected zone using a clip-on strain gage with a gage length of 200 mm. Test machine piston position was also monitored. The instrumentation setup is schematically illustrated in Figure 2.

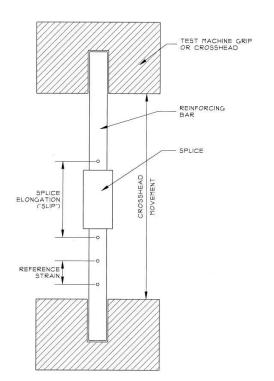


Figure 2. Schematic illustration of test instrumentation setup.

Compression loads and target displacements for Stages 1 and 2 were programmed into the test machine controller, which was operated under a hybrid displacement control/load control. The compression load in all cyclic load stages was set to $0.5*(A_n*R_{eH, spec})$, where A_n is the nominal bar area and $R_{eH, spec}$ is the specified minimum yield strength of 460 MPa. The displacement targets for Stages 1 and 2 (2 $\varepsilon_y L_g$ and 5 $\varepsilon_y L_g$, respectively) were determined using the calculated nominal yield strain and the instrument gage length specified in Section 5.1 of ISO 15835-2.

After Stages 1 and 2 of cyclic loading, each splice specimen was monotonically loaded in tension to failure. The Stage 3 tests were carried out in accordance with ISO 15630-1. The test machine was operated under displacement control during Stage 3. The extensometer remained on the specimen and the elongation (slip) across the splice was recorded during the initial portion of the Stage 3 test to failure. When the test load reached a value of approximately 120 percent of actual bar yield, the LVDT frame was removed from the specimen so that the instrument would not be damaged when the specimen fractured. Similarly, the reference strain was also



recorded as far into Stage 3 as was practicable. For safety purposes, the test machine was temporarily paused with displacement held constant when an instrument was removed from the test specimen. After removal of the instrumentation, displacement was increased until the specimen fractured. Test machine piston position was monitored by computer throughout the test, up to and including specimen fracture. The peak load indicated by the test machine and the observed type of fracture were recorded for each specimen. Corresponding stresses were determined using the nominal bar area. Total elongation at maximum force ($A_{\rm gt}$) of the bar away from the mechanical splice was measured after fracture as prescribed in ISO 15630-01 Section 5.3.

Laboratory Accreditation and Test Machine Certification

WJE is an accredited testing laboratory, recognized by International Accreditation Service, Inc. (IAS) under Certificate TL-165. All tests were performed on a 1780 kN Tinus Olsen universal test machine having hydraulic grips. The Tinus Olsen test machine is located at the WJE headquarters office in Northbrook, Illinois. The current calibration certificates are included in Appendix B.

TEST RESULTS

The tests were carried out on December 21 and 22, 2009. All tests were directed by a WJE staff member who is a licensed structural engineer. The results of the tests are described in the following paragraphs.

Unspliced Control Bars

The results of the tests on the unspliced control bars are summarized in Table 3. The reported tensile properties of all specimens conform to the tensile requirements of BS4449:1997 Grade 460 reinforcing bars. Load-elongation curves for all control bar tests can be found in Appendix C.

Splices Tested for Category B Tensile Strength

Results of the tensile tests on bar specimens in accordance with ISO 15835-1 Category B are summarized in Table 4. Load-elongation (load-slip) curves can be found in Appendix D. The breaking strengths, mode of fracture, and measured $A_{\rm gt}$ values of the specimens are also summarized in Table 4. During the monotonic tensile testing to destruction, all specimens fractured in the reinforcing bar in a ductile fashion away from the splice. A photograph of this failure mode is shown in Figure 3.

For recognition under ISO 15835-1, spliced specimens using BS4449 reinforcing bars must develop a breaking strength of at least $R_{eH,spec} \cdot (R_m/R_{eH})_{spec}$. ISO 15835-1 also requires that specimens achieve a ductility of at least 70% of the specified characteristic A_{gt} value of the reinforcing bar. These requirements are summarized in Table 5. All specimens summarized in Table 4 conform to the strength and ductility requirements.

Splices Tested for Category S2 Cyclic Loading

Results of the cyclic tests on spliced bar specimens in accordance with ISO 15835-1 Category S2 are summarized in Table 6. Load-elongation (load-slip) curves can be found in Appendix E. The Stage 3 breaking strengths, mode of fracture and the measured $A_{\rm gt}$ values of the specimens are also noted in Table 6. During the Stage 3 testing to destruction, all specimens fractured in the reinforcing bar in a ductile fashion away from the splice, as was the case for splices tested for Category B tensile strength.





Figure 3. Representative fractured test specimens, showing bar break away from the mechanical splice

For recognition under ISO 15835-1, spliced specimens using BS4449 reinforcing bars must develop a breaking strength of at least $R_{eH,spec} \cdot (R_m/R_{eH})_{spec}$ and a ductility of at 70 percent of the specified characteristic Agt value of the reinforcing ISO 15835-1 also requires that specimens achieve a residual elongation not exceeding 0.3 mm after Stage 1, and not exceeding 0.6 mm after Stage 2. These requirements are summarized in Table 5. All specimens summarized in Table 6 conform to the strength, ductility and elongation requirements residual summarized in Table 5.

APPLICATION TO ACI-318-08 BUILDING CODE

For recognition under the *ACI 318-08*, the Type 1 and Type 2 mechanical splice must conform to the tensile strength requirements found in *ACI 318-08* Chapter 21, "Special Provisions for Seismic Design," which require the use of Type 2 splices in sections of concrete members where yielding of reinforcement is likely to occur as a result of inelastic lateral displacements under earthquake loading. *ACI 318-08*. Section 21.1.6.1 states that a Type 1 splice shall conform to Section 12.14.3.2 which requires that the splice develop in tension and compression at least 125 percent of the specified yield strength of the reinforcing bar. Section 21.1.6.1 states that a Type 2 splice shall conform to the Type 1 requirements but also develop in tension the specified tensile strength of the spliced bar.

ACI 318-08 Section 21.1.5 also specifies that reinforcement in these areas must comply with ASTM A706. Because the Type 1 and Type 2 splices are defined within Chapter 21 of ACI 318, the specified tensile strength of the bar also includes the special requirements of Section 21.1.5. These special requirements for the reinforcing bar therefore carry over to the strength requirements for Type 1 and Type 2 splices.

ASTM A706 Grade 420 reinforcing bar has a specified yield of 420 MPa, and a specified ultimate tensile strength that is the larger of 560 MPa or 1.25 times the actual yield strength of the reinforcing bar. Review of the reinforcing bar data summarized in Table 3 shows that bars in size No. 32 and 40 comply with the mechanical tensile requirements of ASTM A706 Grade 420 reinforcing bar. The reinforcing bar in size No. 20 does not conform to the mechanical tensile strength requirements of ASTM A706 Grade 420.

Based on the reinforcing bar data summarized in Table 3, the Type 1 and Type 2 splice tensile strengths required to conform to *ACI-318-08* are summarized in Table 5. Review of the tensile strengths of the Category B tensile specimens and the Category S2 cyclic specimens in Tables 4 and 6 shows that specimens in size Nos. 20, 32 and 40 exceed the *ACI 318-08* minimum strength requirements for a Type 1 mechanical splice. Specimens in size No. 32 and 40 comply with the *ACI 318-08* minimum strength requirements for a Type 2 mechanical splice.



Splice specimens in size No. 20 do not conform to the minimum strength requirements for a Type 2 mechanical splice because the reinforcing bar used does not conform to the minimum strength requirements for ASTM A706 Grade 420 reinforcing bars. It is our opinion that the splice system in size No. 20 would be able to conform to these requirements had the BS4449 Grade 460B reinforcing bar used actually conformed to the tensile strength requirements of ASTM A706 Grade 420. The failure mode and the performance of the other tested sizes support this conclusion. It is our opinion that specimens in size No. 20, 32 and 40 all comply with the tensile requirements of ACI 318-08 for Type 1 and 2 mechanical splices.

SUMMARY

WJE conducted a series of tests on reinforcing bar mechanical splices for Bar-US Corporation. The tests were conducted on spliced bar specimens in size Nos. 20, 32 and 40 made with the Simgrip LT coupling sleeves (without the locknut) and BS4449:1997 Grade 460B reinforcing bar. During the Category B tensile tests, all splice specimens met or exceeded the strength and ductility requirements of ISO 15835-1. During reversed-load low cycle tests, all specimens survived the Category S2 cyclic loading as prescribed by ISO 15835-2 and satisfied the residual elongation requirements of ISO 15835-1. These specimens were then loaded in monotonic tension to fracture. All Category S2 splice specimens met or exceeded minimum strength and ductility requirements according to provisions of ISO 15835-1.

Additionally, the ultimate tensile strength of splice specimens in size No. 20, 32 and 40 exceeded minimum strength requirements for a Type 1 mechanical splice on Grade 420 reinforcement according to provisions of *ACI 318-08*. The ultimate tensile strength of splice specimens in size No. 32 and 40 exceeded minimum strength requirements for a Type 2 mechanical splice on ASTM A 706 Grade 420 reinforcement according to provisions of *ACI 318-08*. It is our opinion that the splice specimens in size No. 20 would also have exceed minimum strength requirements for a Type 2 mechanical splice had the specimens been fabricated with reinforcing bar that conformed to ASTM A706 Grade 420 tensile strength requirements.



Table 3 - Control Bar Test Results

Test I.D. Number	Bar Size	Bar Area	Specified Bar Yield Strength	Specified Tensile/Yield	Specified A_{gt}		ield ength	Yield Strain	Tensil	le Strength	(R _m /		
			(R _{eH, spec})	$(\mathbf{R}_{\mathrm{m}}/\mathbf{R}_{\mathrm{eH}})_{\mathrm{spec}}$		F _{eH}	(R _{eH})	ε _y		(R _m)	R _{eH})	$\mathbf{A}_{\mathbf{gt}}$	\mathbf{A}_{5}
	(mm)	(mm ²)	(MPa)	(min)	(percent)	(kN)	(MPa)	(percent)	(kN)	MPa		(percent)	(percent)
3774	20	314	460	1.08	5	159.0	506.4	0.33	191.2	608.9	1.20	9%	24%
3770	32	804	460	1.08	5	391.0	486.3	0.30	507.4	631.1	1.30	10%	25%
3769	40	1257	460	1.08	5	603.0	479.7	0.32	793.7	631.4	1.32	11%	20%

Table 4 - Category B Splice Tensile Test Results

Test	Bar	Bar	Bar	_ •	Strength			
I.D. Number	Size	Area	Grade			$\mathbf{A}_{\mathbf{gt}}$	R_{m}/R_{eH}	Final Result
Number				\mathbf{F}_{\max}	$(\mathbf{R}_{\mathbf{m}})$		K _m ∕ K _e H	Tinai Kesuit
	(mm)	(mm ²)		(kN)	MPa	(percent)		
3775	20	314	460B	191.75	610.7	9.7%	1.21	Bar break
3776	20	314	460B	190.8	607.6	10.8%	1.20	Bar break
3777	20	314	460B	191.7	610.5	10.6%	1.21	Bar break
3760	32	804	460B	506.8	630.3	11.7%	1.30	Bar break
3761	32	804	460B	506.8	630.3	14.5%	1.30	Bar break
3764	32	804	460B	507.7	631.5	10.1%	1.30	Bar break
3762	40	1257	460B	788.1	627.0	10.1%	1.31	Bar break
3763	40	1257	460B	789.8	628.3	10.5%	1.31	Bar break
3765	40	1257	460B	793.1	630.9	10.0%	1.32	Bar break



Table 5 - ISO 15835-1 Requirements for Mechanical Splices

	Reinfo	0	Specified Proper 197 GR460B)	ties	ISO 15835-1 Mecl R	hanical Splice S equirements	System Te	nsile		18-08 Tensil Grade 420 I	-	
Bar	Bar								Type 1		Type 2	
Size	Area	Specified Yield Strength	Specified Tensile/Yield Ratio	$\begin{array}{c} \textbf{Specified} \\ \textbf{A}_{gt} \end{array}$	Tensile Strength: Section 5.2.2	Tensile Ductility: Section 5.2.3	S2 Cy Resid Elonga Section	dual ation:	125% Specified Yield	100% Specified Ultimate	125% Actual Yield	Larger of
(mm)	(mm ²)	(R _{eH}) _{spec} (MPa)	$(R_{\rm m}/R_{\rm eH})_{\rm spec}$	(percent)	$egin{aligned} \mathbf{R_{eH,spec}} * & (\mathbf{R_m}/\mathbf{R_{eH}})_{spec} \ & \mathbf{MPa} \end{aligned}$	A _{gt} (min)	(max) (mm)	u ₈ (max) (mm)	(MPa)	(MPa)	(MPa)	(MPa)
20	314	460	1.08	5	496.8	3.5	0.3	0.6	525	550	633.0	633.0
	514	400	1.08	3	490.8	3.3	0.3	0.0				
32	804	460	1.08	5	496.8	3.5	0.3	0.6	525	550	607.9	607.9
40	1257	460	1.08	5	496.8	3.5	0.3	0.6	525	550	599.6	599.6

Table 6 - Category S2 Splice Low Cycle Test Results

Test I.D.	Bar Size	Bar Area	Bar Grade	Stage 1	Stage 2	Tensile	Strength	$\mathbf{A}_{\mathbf{gt}}$		idual gation		
Number				$2\epsilon_{ m y} { m L}_{ m g}$	$5\epsilon_{ m y} { m L_g}$	\mathbf{F}_{max}	$(\mathbf{R}_{\mathbf{m}})$	(percent)	$\mathbf{u_4}$	$\mathbf{u_8}$	R_m/R_{eH}	Final Result
	(mm)	(mm ²)		Cycles Applied	Cycles Applied	(kN)	MPa		(mm)	(mm)		
3778	20	314	460B	4	4	192.3	612.4	9%	0.02	0.12	1.21	Bar break
3779	20	314	460B	4	4	192.4	612.9	9%	0.01	0.08	1.21	Bar break
3780	20	314	460B	4	4	192.8	614.0	9%	0.03	0.13	1.21	Bar break
3771	32	804	460B	4	4	509.5	633.7	10%	0.19	0.47	1.30	Bar break
3772	32	804	460B	4	4	508.3	632.2	12%	0.15	0.36	1.30	Bar break
3773	32	804	460B	4	4	509.9	634.2	11%	0.15	0.37	1.30	Bar break
3766	40	1257	460B	4	4	784.3	623.9	10%	0.11	0.37	1.30	Bar break
3767	40	1257	460B	4	4	786.6	625.8	10%	0.20	0.47	1.30	Bar break
3768	40	1257	460B	4	4	786.8	625.9	11%	0.14	0.45	1.30	Bar break



APPENDICES



APPENDIX A Reinforcing Bar Mill Certificates



KROMAN KANGAL HADDEHANESI

KALITE BELGESI

QUALITY CERTIFICATE

TARIH

: 18/12/09

REV. NO : 00

FIRMA

BAR-US CORP

BUYER

SIPARIS NO

ORDER NO

BELGE NO

28-0402

DOCUMENT NO

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	· · · · ·	× 6 0		CHEMICAL COMPOSITION IN PRODUCT							MECHANICAL PROPERTIES					
DOKŮ M NO	KALİTE	KESIT	BOY	С	Mn	Si	S	P	Cu	CE	ReH	RM	Α	Oran	Eğme	
(Heat)	(Quality)	(Size)	(Length)	%	%	%	%	%	%	%	N/mm2	N/mm2	%			
39-9 257-0	BS4449	20 Ø	12,00	0,22	0,63	0,19	0,035	0,012	0,26	0,36	573	658	17	1,15	OK	
29 -9257-1	BS4449	. 25 Ø	12,00	0,21	0,63	0,20	0,032	0,014	0,30	0,36	501	649	19	1,30	OK	
29-9 257-2	BS4449	32 Ø	12,00	0,23	0,97	0,33	0,028	0,018	0,24	0,43	523	. 657	15	1,26	OK	
29 -9257-3	BS4449	40 Ø	12,00	0,24	0,96	0,29	0,019	0,016	0,28	0,44	597	737	16	1,23	OK	
29-9257-4	BS4449	16 Ø	12,00	0,20	0,57	0,20	0,026	0,009	0,25	0,34	519	. 622	22	1,20	OK	

ReH: Üst Akma Sınırı [Yield Strength] Rm : Çekme Day. [Tensile Strength] % A : Kopma Uzaması [Elongation] TEST STANDART_ TS 138/EN 10002-1

Ü.P. KALİTE MÜDÜRLÜĞÜ



AŞIROĞLU CAD,NO:175 ÇAYIROVA - GEBZE / KOCAELÎ P.K. 24. 41100 ÇAYIROVA-GEBZE / KOCAELÎ TEL.: 0(262) 679 20 00 FAKS: 0(262) 653 26 76



APPENDIX B Test Machine Current Calibration Certificate



MTS Systems Corporation

14000 Technology Drive Eden Prairie, MN 55344-2290



MTS Field Service

Certificate of Calibration

Customer

Name: Wiss, Janney, Elstner Associates, Inc.

Page: 1 of 4

Certificate Number: 2394-4590

System: Tinius Olsen 114585

Site: 508308

System ID: Tinius Olsen 114585

Location: Structural Lab

Country Code: USA

Equipment

Device Type: Force

Model: REVERE_400KIP

Serial No.: 665148

Controller/Conditioner Model: 493.21B

Serial No.: 1070201

Readout Device Model: 493,21B

Serial No.: 1070201

Channel: Force

MTS Field Service is accredited by the American Association for Laboratory Accreditation (A2LA Cert. No. 1145.01).

The basis for this accreditation is the international standard for calibration laboratories, ISO/IEC 17025

"General Requirements for the Competence of Calibration and Testing Laboratories".

Defined and documented measurement assurance techniques or uncertainty analyses are used to verify the adequacy of the measurement processes.

Calibrations are performed with standards whose values and measurements are traceable to the National Institute of Standards and Technology. MTS Reference Force Transducers are calibrated in compliance with ASTM E74.

When parameter(s) are certified to be within specified tolerance(s), the measured value(s) shall fall within the appropriate specification limit and the uncertainty of the measured value(s) shall be stated and provided to the customer for evaluation.

CALIBRATION INFORMATION

As Found: As Left:

In Tolerance In Tolerance Max. Error As Found: Max. Error As Left:

-0.62 % -0.42 % Calibration Date: Calibration Due:

3-Sep-09 3-Sep-10

Tolerance:

+/-1.0% of Applied Force

FS-CA 2122 Rev. A

ASTM E4-09

Calibration Procedure: Full Scale Ranges:

400000 lbf, 100000 lbf

Note:

STANDARDS USED FOR CALIBRATION

MTS Asset Number	Manufacturer	Model Number	Description	Cal. Date	Cal. Due
16120	Interface Inc.	9840	Interface Box	23-Sep-08	23-Sep-09
17140	Fluke	189	DMM	6-Jul-09	6-Jul-10
15216	FLUKE	80T-150U	TEMP PROBE	23-Sep-08	23-Sep-09
16197	Interface	CX-0330-1	Standarizer	23-Sep-08	23-Sep-09
18178	Strainsense	500 Kip	500 Kip Load Cell	18-May-09	18-May-10
18178_1	Strainsense	500 kip	500kip load cell	18-May-09	18-May-10

Certified by: Jan Thur

Issued on:

3-Sep-09

ACS Version: 7.02

ACSRepRevU GLD 14-Jul-09



Calibration Report



CALIBRATION CERT #1145.01

Customer

Name: Wiss, Janney, Elstner Associates, Inc.

System: Tinius Olsen 114585

Page: 4 of 4

Report Number: 2394-4590

Site: 508308

System ID: Tinius Olsen 114585

Location: Structural Lab

Country Code: USA

Equipment

Device Type: Force

Model: REVERE_400KIP

Serial No.: 665148

Controller/Conditioner Model: 493.21B Readout Device Model: 493.21B Serial No.: 1070201 Serial No.: 1070201

Channel: Force

Procedure

MTS Procedure: FS-CA 2122 Rev. A

ACS Version: 7.02

Calibration has been performed in accordance with:

ASTM E4-09

Method of Verification: Set-the-Force Method using Elastic Calibration Devices Calibration Equipment Asset No.

Dead Weight Set:

HighLevel Board:

LowLevel Board:

Standard Asset No.: 18178

DW Compensation:

DMM: 17140

Digital Indicator: 16120

Lower Limit: 28990 lbf

Temperature Readout: 15216

Additional Equipment:

Standardizer: 16197

Conditions

Ambient Temperature:

72.70 °F

Polarity(+): Tension

Bidirectional:

Cable Length:

25 Feet

In Tolerance

-290914

As Found:

Tolerance: +/-1.0% of Applied Force As Found System Condition:

Good

Out of Tolerance Conditioner Parameters

10.0000

As Adjusted:

1.0017

Delta K:

Negative:

Zero Offset: Range Gain:

0.0000 Multiplier: PreAmp Gain:

260

Cal Res: Post Amp/FineGain:

kohms 1.29016 Polarity:

Inverted

Excitation: Shunt Cal: Positive **Calibration Data**

Range:

Full Scale: 400000

Compression Resolution: 210

Applied	Seri	es 1		Series 1	Errors		Seri	es 2		Series 2	Errors		Rep	eatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		ercent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	-63.0	0.0	0.00	63.0	-0.02	0.0	-48.0	0.0	0.00	48.0	-0.01	0.00	0.00
-20	-80029.0		29.0	0.04			-80035.0		35.0	0.04			0.01	
-40	-159960.0		40.0	-0.03			-159960.0		40.0	-0.03			0.00	
-60	-239810.0		190.0	-0.08			-239800.0		200.0	-0.08			0.00	
-80	-319590.0		410.0	-0.13			-319590.0		410.0	-0.13			0.00	
-100	-399260.0		740.0	-0.19			-399250.0		750.0	-0.19			0.00	
														

Tension

Range:

Applied	Seri	es 1		Series 1	Errors		Seri	es 2		Series 2	Errors		Rep	eatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		ercent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	125.0	0.0	0.00	125.0	0.03	0.0	69.0	0.0	0.00	69.0	0.02	0.00	0.01
20	79929.0		71,0	-0.09			79898.0		102.0	-0.13			0.04	
40	159980.0		20.0	-0.01			159950.0		50.0	-0.03			0.02	
60	240120.0		120.0	0.05			240080.0		80.0	0.03			0.02	
80	320330.0		330.0	0.10			320280.0		280.0	0.09			0.02	
100	400680.0		680.0	0.17			400630.0		630.0	0.16			0.01	
									- V					
- 12														

Errors at Zero are computed in % of Range.

Uncertainty of the data supplied is equal to or less than ±0.25% of reading for a confidence level of 95%.

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American Association of Laboratory Accreditation Certificate Number: 1145.01

MTS Reference Force Transducers are temperature compensated over the range of use

Performed By:

James Rieder

Field Service Engineer

Date: 3-Sep-09

For Tud

Next Customer Agreed Upon Calibration Date:

3-Sep-10

ACSRepRevU GLD 14-Jul-09

Out of Tolerance in % column



Calibration Report



Customer

Name: Wiss, Janney, Elstner Associates, Inc.

Method of Verification: Set-the-Force Method using Elastic Calibration Devices

System: Tinius Olsen 114585

Page: 2 of 4

CALIBRATION CERT #1145.01

Report Number: 2394-4590 Site: 508308

System ID: Tinius Olsen 114585

Location: Structural Lab

Country Code: USA

Equipment

Device Type: Force

Model: REVERE_400KIP

Serial No.: 665148

Controller/Conditioner Model: 493.21B Readout Device Model: 493.21B Serial No.: 1070201 Serial No.: 1070201

Channel: Force

Procedure

MTS Procedure: FS-CA 2122 Rev. A

ACS Version: 7.02

Calibration has been performed in accordance with:

ASTM E4-09

Calibration Equipment Asset No.

Dead Weight Set:

HighLevel Board:

LowLevel Board:

Standard Asset No.: 18178

DW Compensation:

DMM: 17140

Digital Indicator: 16120

Lower Limit: 28990 lbf

Temperature Readout: 15216

Additional Equipment:

Standardizer: 16197

Conditions

Ambient Temperature:

0.00 °F

Polarity(+): Tension

Bidirectional:

Cable Length:

25 Feet

in Tolerance

X

As Found: As Adjusted: Tolerance: +/-1.0% of Applied Force As Found System Condition:

Good

Out of Tolerance

Conditioner Parameters 10.0000

Delta K: 0.9963

Zero Offset: Range Gain:

0.0000 Multiplier: PreAmp Gain:

260

Cal Res: Post Amp/FineGain:

kohms Polarity: 1.29141

Inverted

Shunt Cal: Calibration Data

Excitation:

Positive

-290914 Range: Resolution:

Negative: 210

Full Scale: 400000

Compression

Applied	Seri	es 1		Series 1	Errors		Seri	es 2		Series 2	Errors		Rep	eatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	-106.0	0.0	0.00	106.0	-0.03	0.0	-48.0	0.0	0.00	48.0	-0.01	0.00	0.01
-20	-79706.0		294.0	-0.37			-79691.0		309.0	-0.39			0.02	
-40	-159280.0		720.0	-0.45			-159260.0		740.0	-0.46			0.01	
-60	-238790.0		1210.0	-0.50			-238730.0		1270.0	-0.53			0.03	
-80	-318210.0		1790.0	-0.56			-318220.0		1780.0	-0.56			0.00	
-100	-397520.0		2480.0	-0.62			-397510.0		2490.0	-0.62			0.00	

Tension Report Units Range:

Applied	Seri	es 1		Series 1	Errors		Seri	es 2		Series 2	Errors		Rep	eatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	130.0	0.0	0.00	130.0	0.03	0.0	74.0	0.0	0.00	74.0	0.02	0.00	0.01
20	79998.0		2.0	0.00			79977.0		23.0	-0.03			0.03	
40	160120.0		120.0	0.08			160080.0		80.0	0.05	11000		0.03	
60	240330.0		330.0	0.14			240290.0		290.0	0.12			0.02	
80	320620.0		620.0	0.19			320580.0		580.0	0.18			0.01	
100	401070.0		1070.0	0.27			401000.0		1000.0	0.25			0.02	
				SOURCE LO		-			_					
	-			×							E 245			-

Errors at Zero are computed in % of Range.

Uncertainty of the data supplied is equal to or less than ±0.25% of reading for a confidence level of 95%.

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American Association of Laboratory Accreditation Certificate Number: 1145.01

MTS Reference Force Transducers are temperature compensated over the range of use

Performed By:

James Rieder

Field Service Engineer

Date:

3-Sep-09

Next Customer Agreed Upon Calibration Date:

3-Sep-10

ACSRepRevU GLD 14-Jul-09

Out of Tolerance in % column



Calibration Report



CALIBRATION CERT #1145.01

Customer

Name: Wiss, Janney, Elstner Associates, Inc.

System: Tinius Olsen 114585

Page: 3 of 4

Report Number: 2394-4590

Site: 508308

System ID: Tinius Olsen 114585

Location: Structural Lab

Country Code: USA

Equipment

Device Type: Force

Model: REVERE_400KIP

Serial No.: 665148

Controller/Conditioner Model: 493.21B Readout Device Model: 493.21B

Serial No.: 1070201 Serial No.: 1070201

Channel: Force

Procedure

MTS Procedure: FS-CA 2122 Rev. A

ACS Version: 7.02

Calibration has been performed in accordance with:

ASTM E4-09 Method of Verification: Set-the-Force Method using Elastic Calibration Devices

Calibration Equipment Asset No.

10.0000

Dead Weight Set:

HighLevel Board:

LowLevel Board:

Standard Asset No.: 18178_1

DW Compensation:

DMM: 17140

Digital Indicator: 16120

Lower Limit: 10000 lbf

Temperature Readout: 15216

Additional Equipment:

Standardizer: 16197

Conditions

Ambient Temperature:

72.30 °F

Polarity(+): Tension Х

Bidirectional:

Cable Length:

25 Feet

In Tolerance

As Found:

Tolerance: +/-1.0% of Applied Force As Found System Condition:

Good

Out of Tolerance Conditioner Parameters

As Adjusted:

1.0012

Delta K:

Zero Offset: Range Gain:

0.0000 Multiplier: PreAmp Gain:

Cal Res: 260 Post Amp/FineGain:

kohms 5.15438 Polarity: Inverted

Positive: Shunt Cal: **Calibration Data**

Excitation:

Negative: Range: Resolution: 21.6

Full Scale: 100000

Compression Report Units

Applied	Seri	ies 1		Series 1	Errors		Seri	es 2		Series 2	Errors		Rej	peatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	-41.6	0.0	0.00	41.6	-0.04	0.0	-35.0	0.0	0.00	35.0	-0.04	0.00	0.01
-20	-19957.0		43.0	-0.22	8	1818	-19948.0		52.0	-0.26			0.05	
-40	-39902.0		98.0	-0.25			-39897.0		103.0	-0.26			0.01	
-60	-59853.0		147.0	-0.25			-59839.0		161.0	-0.27			0.02	
-80	-79802.0		198.0	-0.25			-79791.0		209.0	-0.26			0.01	
-100	-99744.0		256.0	-0.26			-99727.0		273.0	-0.27			0.02	
													- 0	
					-									
		1		22 1										

Tension Report Units Range:

Applied	Ser	ies 1		Series 1	Errors		Ser	ies 2		Series 2	Errors		Re	peatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Force	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.0	38.5	0.0	0.00	38.5	0.04	0.0	17.3	0.0	0.00	17.3	0.02	0.00	0.02
20	19919.0		81.0	-0.41	150		19919.0		81.0	-0.41			0.00	
40	39838.0		162.0	-0.41			39833.0		167.0	-0.42			0.01	
60	59759.0		241.0	-0.40			59758.0		242.0	-0.40			0.00	
80	79701.0		299.0	-0.37			79686.0		314.0	-0.39			0.02	200
100	99634.0		366.0	-0.37			99630.0		370.0	-0.37			0.00	
0.1							-						- 1	-
				-5	-									
		- N - 175											بأرديب	_

Errors at Zero are computed in % of Range.

Uncertainty of the data supplied is equal to or less than $\pm 0.25\%$ of reading for a confidence level of 95%.

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Calibrations are performed with standards whose values and measurements are traceable to the National Institute of Standards and Technology.

American Association of Laboratory Accreditation Certificate Number: 1145.01

MTS Reference Force Transducers are temperature compensated over the range of use.

Performed By:

James Rieder

Field Service Engineer

Date:

3-Sep-09

Som Per Signature:

Next Customer Agreed Upon Calibration Date:

3-Sep-10

ACSRepRevU GLD 14-Jul-09

Out of Tolerance in % column



MTS Systems Corporation

14000 Technology Drive Eden Prairie, MN 55344-2290



MTS Field Service

Certificate of Calibration

Customer

Page: 1 of 2

Name: Wiss, Janney, Elstner Associates, Inc.

Certificate Number: 2394-4591

System ID: Tinius Olsen 114585

System: Tinius Olsen 114585 Location: Structural Lab

Site: 508308 Country Code: USA

Equipment

Device Type: Length

Model: COLLINS_LVDT

Serial No.: 572988

Controller/Conditioner Model: 493.21B

Serial No.: 10-70206

Readout Device Model: 493,21B

Serial No.: 10-70206

Channel: Displacement

MTS Field Service is accredited by the American Association for Laboratory Accreditation (A2LA Cert. No. 1145.01). The basis for this accreditation is the international standard for calibration laboratories, ISO/IEC 17025 "General Requirements for the Competence of Calibration and Testing Laboratories". Defined and documented measurement assurance techniques or uncertainty analyses are used to verify the adequacy of the measurement processes.

Calibrations are performed with standards whose values and measurements are traceable to the National Institute of Standards and Technology.

When parameter(s) are certified to be within specified tolerance(s), the measured value(s) shall fall within the appropriate specification limit and the uncertainty of the measured value(s) shall be stated and provided to the customer for evaluation.

CALIBRATION INFORMATION

As Found:

In Tolerance

Max. Error As Found:

0.10 %

Calibration Date:

3-Sep-09

As Left:

In Tolerance

Max. Error As Left:

0.10 %

Calibration Due:

3-Sep-10

+/-1.0% of Range Tolerance:

Calibration Procedure:

FS-CA 2124 Rev. A

Full Scale Ranges:

6 inch

Note:

STANDARDS	USED FOR	CALIBRATIO	N

MTS Asset Number	Manufacturer	Model Number	Description	Cal. Date	Cal. Due
17140 15216	Fluke FLUKE	189 80T-150U	DMM TEMP PROBE	6-Jul-09 23-Sep-08	6-Jul-10 23-Sep-09
19739	Boeckeler (9 pin)	DLG 460	Digital Linear Scale	12-Jan-09	12-Jan-10

Certified by: for Lud

Issued on:

3-Sep-09

ACS Version: 7.02

ACSRepRevU 14-Jul-09



Calibration Report



CALIBRATION CERT #1145.01

Customer

Name: Wiss, Janney, Elstner Associates, Inc.

System: Tinius Olsen 114585

Page: 2 of 2

Report Number: 2394-4591

Site: 508308

System ID: Tinius Olsen 114585

Location: Structural Lab

Country Code: USA

Equipment

Device Type: Length

Model: COLLINS_LVDT

Serial No.: 572988

Controller/Conditioner Model: 493.21B Readout Device Model: 493.21B Serial No.: 10-70206 Serial No.: 10-70206

Channel: Displacement

Procedure

MTS Procedure: FS-CA 2124 Rev. A

ACS Version: 7.02

Calibration has been performed in accordance with:

(none)

Method of Verification:

Calibration Equipment Asset No.

Dead Weight Set:

HighLevel Board:

LowLevel Board:

Standard Asset No.: 19739

DW Compensation:

DMM: 17140

Digital Indicator:

Lower Limit:

Temperature Readout: 15216

Additional Equipment:

Standardizer:

Conditions

Ambient Temperature: 72.80 °F Polarity(+): Retraction

Bidirectional:

Cable Length:

25 Feet

Polarity:

In Tolerance **Out of Tolerance**

X

As Found:

Tolerance: +/-1.0% of Range As Found System Condition:

Good

Conditioner Parameters Excitation: 10.0002

Delta K: 1.0021

Zero Offset: Range Gain: 0.0000

Multiplier: PreAmp Gain: Post Amp/FineGain:

43.59375 0.96883

Inverted

Cal Factor: **Calibration Data** Extension

Positive: Range: Resolution:

Negative: 0.012

Full Scale:

As Adjusted:

Applied	Ser	ies 1		Series	1 Errors		Ser	ies 2		Series 2	Errors		Rep	eatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Length	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
Õ	0.00000	-0.00023	0.00000	0.00	0.00023	0.00								
-10	-0.60105		0.00105	0.02										
-20	-1.20210		0.00210	0.04										
-40	-2.40600		0.00600	0.10				1						
-50	-3.00190		0.00190	0.03										
-60	-3.60560		0.00560	0.09										
- 1														
	1.12													
														100

Retraction

Range:

Applied	Ser	ies 1		Series	1 Errors		Ser	ies 2		Series 2	Errors		Re	peatability
Percent of Full Scale	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error	Indicated Reading	Indicated Reading	Units Error	Percent Error	Units Error	Percent Error		Percent Error
Length	Ascending	Descending	Asc	Asc	Desc	Desc	Ascending	Descending	Asc	Asc	Desc	Desc	Asc	Desc
0	0.00000	-0.00001	0.00000	0.00	0.00001	0.00								
10	0.59798		0.00202	-0.03										
20	1.19670		0.00330	-0.06										
40	2.39830		0.00170	-0.03										
50	2.99940		0.00060	-0.01										
60	3.60320		0.00320	0.05										
										-			-	
							1-500							

Uncertainty of the calibration data supplied is equal to or less than the greater of, ±0.25% of reading or ±50µ inches, for a confidence level of 95%. This report shall not be reproduced except in full, without the written approval of the laboratory.

Out of Tolerance in % column

Calibrations are performed with standards whose values and measurements are traceable to the National Institute of Standards and Technology. American Association of Laboratory Accreditation Certificate Number: 1145.01

Notes:

Performed By:

James Rieder

Field Service Engineer

Date:

3-Sep-09

In Zeel Signature:

Next Customer Agreed Upon Calibration Date:

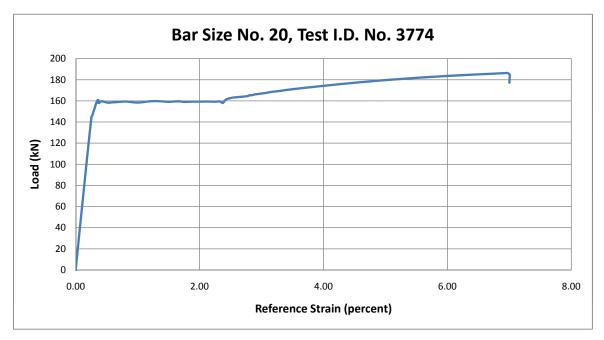
3-Sep-10

ACSRepRevU GLD 14-Jul-09



APPENDIX C Control Bar Load-Elongation Curves

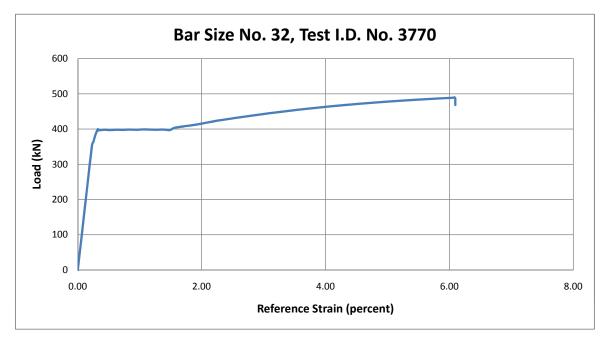
Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)		trength, _{eH}	Yield Strain,	Tensile S	Strength	A _{gt} (percent)	A ₅ (percent)
				(kN)	(MPa)	ε _{ya} (percent)	(kN)	(MPa)		
3774	20	A	314	159.0	506.4	0.33%	191.2	608.9	9%	20%





Wiss, Janney, Elstner Associates, Inc. 10 S. LaSalle Street, Suite 2600 Chicago, Illinois 60603 312.372.0555 tel | 312.372.0873 fax www.wie.com

Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)		trength, _{eH}	Yield Strain,	Tensile S	Strength	A _{gt} (percent)	A ₅ (percent)
				(kN)	(MPa)	ε _{ya} (percent)	(kN)	(MPa)		
3770	32	A	804	391.0	486.3	0.30%	507.4	631.1	10%	25%





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Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)		trength, _{eH}	Yield Strain,	Tensile S	Strength	A _{gt} (percent)	A ₅ (percent)
				(kN)	(MPa)	ε _{ya} (percent)	(kN)	(MPa)		
3769	40	A	1257	603.0	479.7	0.32%	793.7	631.4	11%	20%



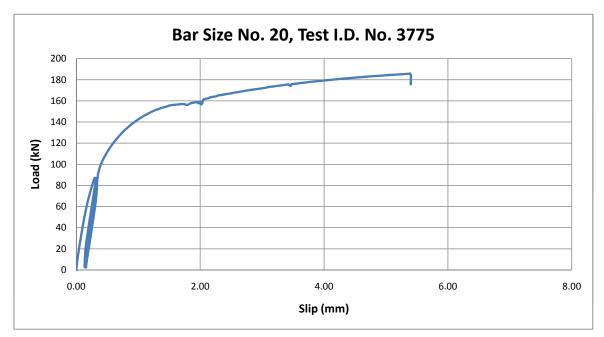


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APPENDIX D
Splice Specimens Load-Slip Curves for Category B TensileTesting Protocol

Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3775	20	A	314	191.8	610.7	10%	Bar break





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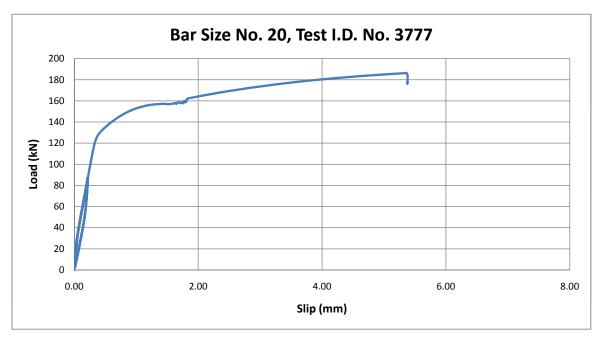
Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3776	20	A	314	190.8	607.6	11%	Bar break





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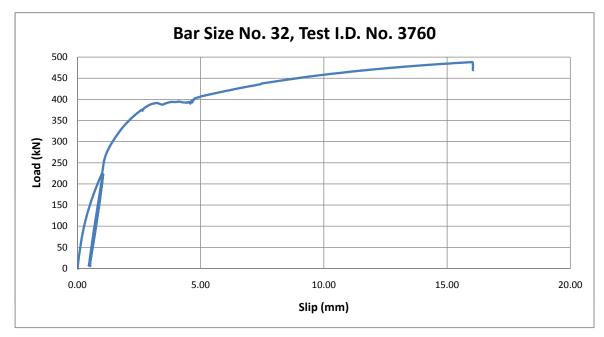
Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3777	20	A	314	191.7 610.5		11%	Bar break





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Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3760	32	A	804	506.8 630.3		12%	Bar break





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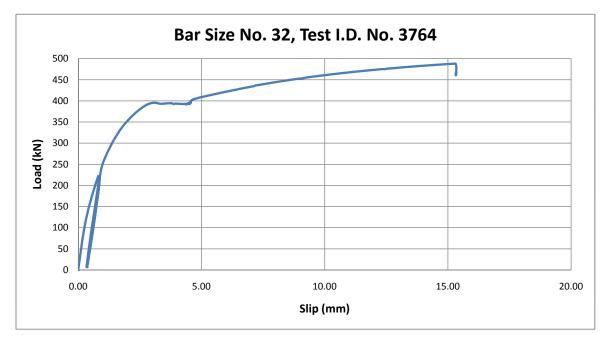
Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3761	32	A	804	506.8 630.3		15%	Bar break





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Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3764	32	A	804	507.7 631.5		11%	Bar break





Wiss, Janney, Elstner Associates, Inc. 10 S. LaSalle Street, Suite 2600 Chicago, Illinois 60603 312.372.0555 tel | 312.372.0873 fax www.wje.com

Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3762	40	A	1257	788.1 627.0		10%	Bar break





Wiss, Janney, Elstner Associates, Inc. 10 S. LaSalle Street, Suite 2600 Chicago, Illinois 60603 312.372.0555 tel | 312.372.0873 fax www.wje.com

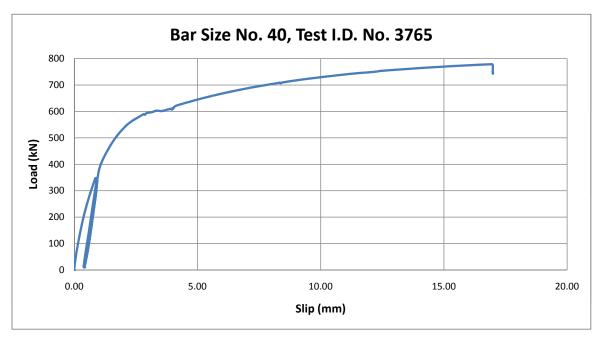
Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Strength	A _{gt} (percent)	Final Result
				(kN)	(MPa)		
3763	40	A	1257	789.8 628.3		10%	Bar break





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Test I.D. No.	Bar Size	Bar Lot	Bar Area (mm²)	Tensile S	Tensile Strength		Final Result
				(kN)	(MPa)		
3765	40	A	1257	793.1 630.9		10%	Bar break





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APPENDIX E Splice Specimens Load-Slip Curves for Category S2 Testing Protocol

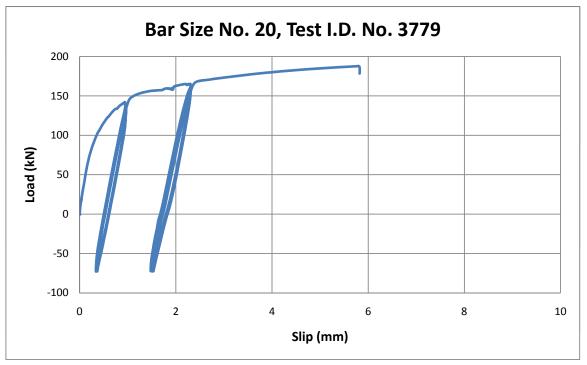
Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2		Residual Elongation				Final Result
	(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$\begin{array}{c} 2_{\epsilon y}L_g\\ Cycles\\ Applied \end{array}$	$\begin{array}{c} \mathbf{5_{Ey}L_g} \\ \mathbf{Cycles} \\ \mathbf{Applied} \end{array}$	u ₄ (mm)	u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
3778	20	314	A	460	4	4	0.02	0.12	192.3	612.4	9%	Bar break





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	Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2		dual gation			$\mathbf{A_{gt}}$	Final Result
		(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$egin{array}{c} 2_{\mathrm{gy}} \mathrm{L_{g}} \\ \mathrm{Cycles} \\ \mathrm{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$		u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
ľ	3779	20	314	A	460	4	4	0.01	0.08	192.4	612.9	9%	Bar break





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Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2		Residual Elongation				Final Result
	(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$\begin{array}{c} 2_{\text{gy}} L_{\text{g}} \\ \text{Cycles} \\ \text{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$		u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
3780	20	314	Α	460	4	4	0.03	0.13	192.8	614.0	9%	Bar break





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	Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2		dual gation			$\mathbf{A_{gt}}$	Final Result
		(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$egin{array}{c} 2_{\mathrm{gy}} \mathrm{L_{g}} \\ \mathrm{Cycles} \\ \mathrm{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$		u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
Ī	3771	32	804	A	460	4	4	0.19	0.47	509.5	633.7	10%	Bar break





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Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2		Residual Elongation				Final Result
	(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$egin{array}{c} 2_{ m gy} { m L_g} \ { m Cycles} \ { m Applied} \end{array}$	$egin{array}{c} 5_{\epsilon y} L_{g} \ Cycles \ Applied \end{array}$	u ₄ (mm)	u ₈ (mm)	F _{max}	(R _m)	(percent)	
3772	32	804	A	460	4	4	0.15	0.36	508.3	632.2	12%	Bar break





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	Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2	Residual Elongation		Tensile Strength		$\mathbf{A_{gt}}$	Final Result
		(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$egin{array}{c} 2_{\mathrm{gy}} \mathrm{L_{g}} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$	` /	u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
Ī	3773	32	804	Α	460	4	4	0.15	0.37	509.9	634.2	11%	Bar break





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Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2	Residual Elongation		Tensile Strength		$\mathbf{A_{gt}}$	Final Result
	(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$\begin{array}{c} 2_{\text{gy}} L_{\text{g}} \\ \text{Cycles} \\ \text{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$	u ₄ (mm)	u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
3766	40	1257	Α	460	4	4	0.11	0.37	784.3	623.9	10%	Bar break





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	Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2	Residual Elongation		Tensile Strength		$\mathbf{A_{gt}}$	Final Result
		(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$\begin{array}{c} 2_{\text{gy}} L_{\text{g}} \\ \text{Cycles} \\ \text{Applied} \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$		u ₈ (mm)	F _{max} (kN)	(R _m) MPa	(percent)	
I	3767	40	1257	Α	460	4	4	0.20	0.47	784.3	623.9	10%	Bar break





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Test I.D. Number	Bar Size	Bar Area	Bar Lot	Specified Bar Yield Strength	Stage 1	Stage 2	Residual Elongation		Tensile Strength		${f A_{gt}}$	Final Result
	(mm)	(mm ²)		(R _{eH, spec}) (MPa)	$egin{array}{c} 2_{ extsf{ iny Sy}} L_{ extsf{g}} \ Cycles \ Applied \end{array}$	$egin{array}{c} 5_{\mathrm{gy}} \mathrm{L_g} \ \mathrm{Cycles} \ \mathrm{Applied} \end{array}$		u ₈ (mm)	F _{max}	(R _m)	(percent)	
3768	40	1257	A	460	4	4	0.14	0.45	784.3	623.9	A /	Bar break





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